

G. T. SCHJELDAHL COMPANY  
NORTHFIELD, MINNESOTA

January 30, 1963

FINAL REPORT  
EVALUATION OF THE COMPATIBILITY OF  
POLYVINYLIDENE FLUORIDE (KYNAR)  
WITH  
STORABLE LIQUID PROPELLANTS  
(NITROGEN TETROXIDE AND HYDRAZINE)

Prepared for  
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## I. SUMMARY

This final report presents the result of research conducted under the Jet Propulsion Laboratory's Contract No. NI-120420. The objective of this contract was the evaluation of polymeric materials potentially usable to construct expulsion membranes for storable liquid propellants such as nitrogen tetroxide and hydrazine. The material studied was polyvinylidene fluoride available as Kynar from Pennsalt Chemical Company.

The work of others has been reviewed and applied to this study and the aid of materials suppliers has been enlisted whenever possible. The study of polymers was deviated from, in one respect, when some aluminum laminates were prepared for a brief evaluation at Jet Propulsion Laboratory.

The evaluation accomplished at the Schjeldahl Company has been based on 1) preparation of film samples from resins and from resin dispersions and solutions, 2) immersion tests in storable propellants, followed by measuring physical properties of the films and resins, 3) simple permeability tests. In all tests comparison samples of other resin systems were included.

Work since the last formal report has centered around long-term immersion studies and determining polyvinylidene fluoride film characteristics after orienting and stretching procedures.





## II. CONCLUSIONS

1. The polyvinylidene fluoride polymer is unattached chemically by  $N_2O_4$  or Hydrazine. Swelling occurs with  $N_2O_4$  and some brittleness develops on long contact with hydrazine.
2. Solution cast and extrusion were demonstrated for the preparation of film from polyvinylidene fluoride. Sintering of solid material by a fluidized bed technique showed little promise.
3. The suitability of using infrared spectral analysis for establishing physical and chemical interaction between propellant and selected film was demonstrated.
4. The testing conducted with polyvinylidene fluoride and Teflon FEP indicated promise for the former for use in applications of intermittent exposure or where permeability is not an important factor. Consideration should, therefore, be given to its use in O-rings, gaskets, or molded parts.
5. Evidence was obtained to indicate that polyvinylidene fluoride films can be oriented by application of strain at a proper temperature. Sensitivity of the material to melt fracture and to temperature are sufficiently great to indicate that operation within very narrow limits will be necessary.



6. The test methods were suitable for preliminary testing or screening of materials but refinements are needed for definition of long-term behavior of material in contact with storable propellants.
7. Studies of the effect of propellant on polymer molding powder in comparison with biaxially oriented film indicate that the orientation process may reduce susceptibility to attack several fold..

Recommendations:

It is recommended that:

1. Polyvinylidene fluoride be considered for systems involving  $N_2O_4$  where a relatively hard polymer with some permeability is suitable. (Performance anticipated would be equivalent or superior to that of Teflon FEP)
2. Vinylidene fluoride be considered for use in cross-linked polymer systems where resistance to  $N_2O_4$  is important. (The absence of chemical attack and the low order of swelling, point to an excellent potential for reduced swelling. Complete elimination of permeability is not to be anticipated.)



3. Vinylidene fluoride polymers be considered for use in laminated systems where metals are employed to eliminate permeability. (The resistance of the few aluminum laminates prepared with epoxy adhesives under this program indicates the effectiveness of metal barriers for  $N_2O_4$ ).



### III. TECHNICAL DISCUSSION

Through May 1961, work under the contract centered on a brief review of the work of others in the area of storable propellants compatibility. Kynar, vinylidene fluoride, being newly available and promising in preliminary experiments at G. T. Schjeldahl Company was the subject of emphasis. The potential promised that vinylidene fluoride would be comparable to Teflon FEP in compatibility. Suppliers technical product development personnel were interviewed to establish a justification for the study of Kynar as a propellant barrier material. (1)

Following this, a group of materials required for the study was assembled (cylinder  $N_2O_4$ , anhydrous hydrazine, and apparatus). Initial attempts to prepare Kynar film samples were made. Very thin films (0.0005-inch) were cast continuously, heavier sections (0.001- 0.003-inch) were cast in small areas, and plaques (0.25-inch) were compression molded. The greatest difficulties occurred in preparing a uniform plaque, and completely removing the high boiling-point solvents and dispersants used in casting. These samples were, in several ways, exposed to nitrogen tetroxide and hydrazine.

In the period covered by the second report (2) emphasis was again placed on Kynar. Polypropylene, polycarbonate, polyvinylidene chloride polymer and polyethylene were included





in initial immersion tests for comparison. The polyethylene and polycarbonate were attacked on initial immersion in propellants, the polycarbonate being completely decomposed. Films of vinylidene fluoride, vinylidene chloride, and polypropylene were immersed and, on removal, tested for tensile strength, inspected for discoloration (indicating absorption) and the infrared spectra recorded to check for residual solvents and for nitration of the polymer.

The polyvinylidene fluoride films would discolor on immersion but on exposure to air would lose the color. No infrared absorption bands indicated nitration of the polymer. It was noted then that the spectra indicated residual solvents and dispersants. It was assumed that these residuals could have left material which would readily transmit the nitrogen tetroxide. The polypropylene was observed to suffer greater attack on the molding pellets than on the oriented film. After one week, an infrared absorption band indicated some nitration. A 2-oz Boston round bottle of nitrogen tetroxide exuded the material through the wall after a few days. Following this, simple permeation and longer-term and higher temperature immersion tests were run.

The third letter report (3) described simple permeation testing and some 150 F nitrogen tetroxide immersion tests in addition to those already run. At this time, the seemingly delayed attack on biaxially-oriented film compared to polypropy-



lene pellets was noted. Polyvinyl fluoride, polyvinyl chloride copolymer, and polypropylene films and pellets were sealed into glass tubes (15 mm tubes for room temperature, 8 mm tubes for 150 F). After one to two days, the polypropylene pellets at 150 F degraded enough to burst the sample tube. After two to seven days, the biaxially-oriented polypropylene film samples burst the sample tube. (After roughly three months, the polypropylene samples immersed at room temperature burst their sealed tubes.) The vinylidene chloride copolymer and the vinylidene fluoride would regain original physical properties within a day after being removed from the nitrogen tetroxide. Simple permeability studies were made to compare the polyvinylidene film to Teflon FEP. The permeability is almost equal to that of Teflon FEP of similar thicknesses. The immersion and permeability samples of Kynar were prepared from six pounds of film extruded experimentally at the Panelyte division of St. Regis Paper Company at Richmond, Indiana. This eliminated inconsistencies in the sample but it also introduced the problem of melt fractures in the film and very low tensile strength and elongation in the transverse direction of the film.

Long-term exposures were then initiated for the polyvinylidene fluoride and the polyvinylidene chloride polymer in both hydrazine and  $N_2O_4$  sealed in tubes. These sealed tubes have been maintained at room temperature for 13 months.



For two months some small diameter tubes containing  $N_2O_4$  and samples of Kynar and vinylidene chloride copolymer were held at 150 F. Corresponding samples of polypropylene film and resin burst the containing tube. The vinylidene chloride copolymer was degraded and became flaky when removed from the 150 F immersion in  $N_2O_4$ . The Kynar film samples, after being exposed to air for three days had tensile properties approximately the same as control sample. The sample was bleached to a hazy water-white material. It was apparent that in this case  $N_2O_4$  was absorbed in the film. There was not any indication of nitration of the Kynar. Samples of room temperature immersion in hydrazine were yellowed and embrittled slightly after 13 months.

Repeated attempts were made to obtain biaxially oriented Kynar film to evaluate the effect of orientation on permeability. The Kynar film has poor hot strength and all stretching took place from a line of melt fracture. In the extruded film this was always in the machine direction. Within the Schjeldahl Company, the stretching was attempted by drawing in one direction in a frame in the tensile tester, drawing over a sphere (thermo-forming) and by pressing between hot platens. None of these systems offered a suitable sample. The T. M. Long Company, Summerville, New Jersey offered to stretch limited samples.



The film was described by them as being sensitive in one direction and not lending itself to good stretching on the T. M. Long film stretcher. For this reason, the stretched film samples were not of a quality suitable for use as permeability test specimens.





#### IV. RESULTS OF TEST PROGRAMS

The first phase of the work resulted in confirmation of the choice of Kynar as a potential material. The justification is reviewed in the notes of the meeting with Dr. Barnhart of Pennsalt Chemicals Corporation. Dr. Barnhart offered a great deal of information on the handling properties and chemical nature of Kynar. A review with Plastec (Picatinney Arsenal) of an Aerojet General report on the evaluation of elastomeric compounds for use with storable propellants was not entirely applicable because it was concerned more with brief exposure and intermittent service. This report did indicate that Teflon and hexamethylene diamine Nylons are potentially usable but that Teflon usefulness lay in its ability to degas easily what it had absorbed.

During the second phase, films of polyvinylidene fluoride were cast from Kynar dispersions and solutions. It was noted that one could observe residual solvent readily in the infrared spectra of the films. A dispersion of powder in a 80/20 blend of dimethylphthalate and diisobutyl ketone offered some thixotropy and could be considered to stop the running problem experienced when continuous films were cast on the Schjeldahl laminator. Physical properties of Kynar films prepared in this manner were essentially the same as those published earlier.

Initial immersion testing eliminated polycarbonate and vinyl acetate. Polypropylene was later eliminated when higher temperatures (150 F) were used. The spectra of all material samples immersed



in  $\text{N}_2\text{O}_4$  showed an absorption band at  $1550\text{ cm}^{-1}$  which diminished with time. This indicated that absorbed  $\text{N}_2\text{O}_4$  would be completely released on degassing.

It was noted that biaxially oriented polypropylene sheet was less sensitive to  $\text{N}_2\text{O}_4$  degradation than were polypropylene pellets. After 1 week immersion, a permanent absorption band at  $1550\text{ cm}^{-1}$  indicated nitration of polypropylene. Initial permeability tests indicated leakage rather than permeability.

In the third phase of the study, immersion of samples in nitrogen tetroxide was done at 150 F. Polypropylene pellets would break the sample-containing tube in less than 24 hours. Oriented polypropylene film took 48 hours to burst the tube. The Kynar film discolored, indicating absorption. After brief exposure to air, the Kynar films regained original properties. The properties, if tested before degassing, could occur, were

Ultimate Tensile	73 % of original
Ultimate Elongation	10 % of original
Color	Green from original tan.

A sample polyvinylidene fluoride film prepared outside the Schjeldahl Company showed leakage. The high melt viscosity forced open the extruded sheet die to three times original depth. Poor hot strength was observed. Annealing of the sample did little to diminish the effects of melt fracture at the extruder die.



Experimental work has substantiated the difficulty of biaxially orienting Kynar film. Hot stretching in a frame, in the tensile tester, and by drawing over a cone would not stretch the film uniformly. The T. M. Long Company also noted the poor hot strength and the melt fracture problem.

Permeability measurements of Kynar film gave the following results:

<u>Length of Exposure</u> (hrs)	<u>Description of Film</u>	<u>Permeability</u> mg/(mil)(day)(atm)(in <sup>2</sup> )
48	7-mil Kynar	95
100	7-mil Kynar	100
21	7-mil Kynar	100
21	5-mil Teflon FEP(Control)	95

Long-term (13 months) immersion of samples in  $N_2O_4$  and  $N_2H_4$  was carried out. After removal from these conditions, the Kynar film was bleached white by  $N_2O_4$  and stained yellow by the  $N_2H_4$ . The hydrazine also made the film more brittle. Polypropylene was no longer of interest in higher temperature immersion as reaction had already been shown to occur. The vinylidene chloride copolymer was embrittled seriously by the  $N_2O_4$ .



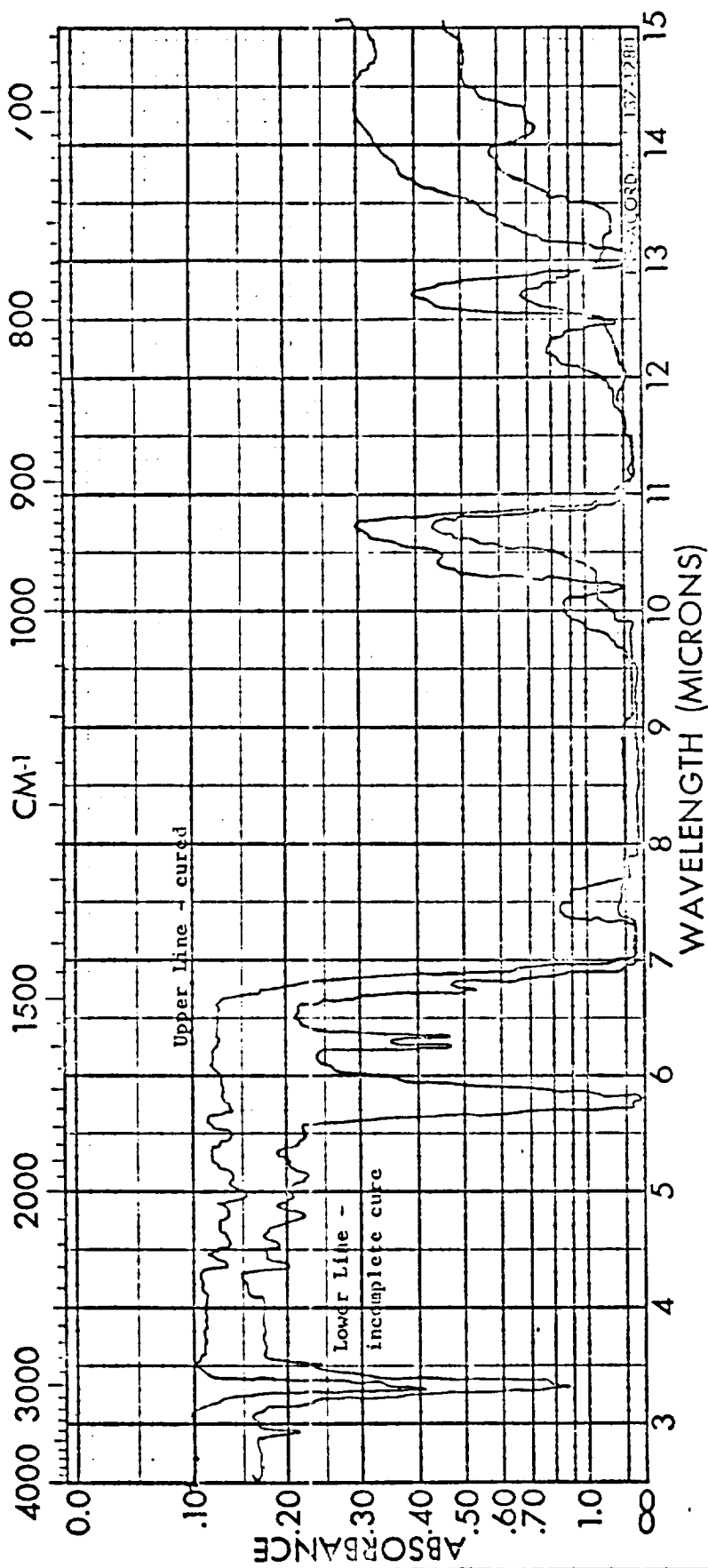
GENERAL RESULTS TABLE

	Polyvinylidene fluoride*	Polyvinylidene chloride	Teflon FEP	Polypropylene	Vinyl Acetate	Polycarbonate
Brief Exposure to $N_2O_4$	Not Affected	Not Affected	Not Affected	Discolored	Decomposed	Decomposed
2 months exposure to $N_2O_4$	Absorbed Discolored No permanent effect			Tank Rupture		
13 months in $N_2O_4$	Absorbed, softened, bleached - no chemical reaction - no effect on tensile strength	Absorbed, some chemical reaction discolored, very brittle	Absorbed, swelled - no chemical reaction	Decomposed		
Brief exposure to hydrazine	Not Affected	No data	Not Affected	No data	No data	No data
Long term exposure to hydrazine	Embrittled, discolored	No data	No data			

\* Extruded Film Sample



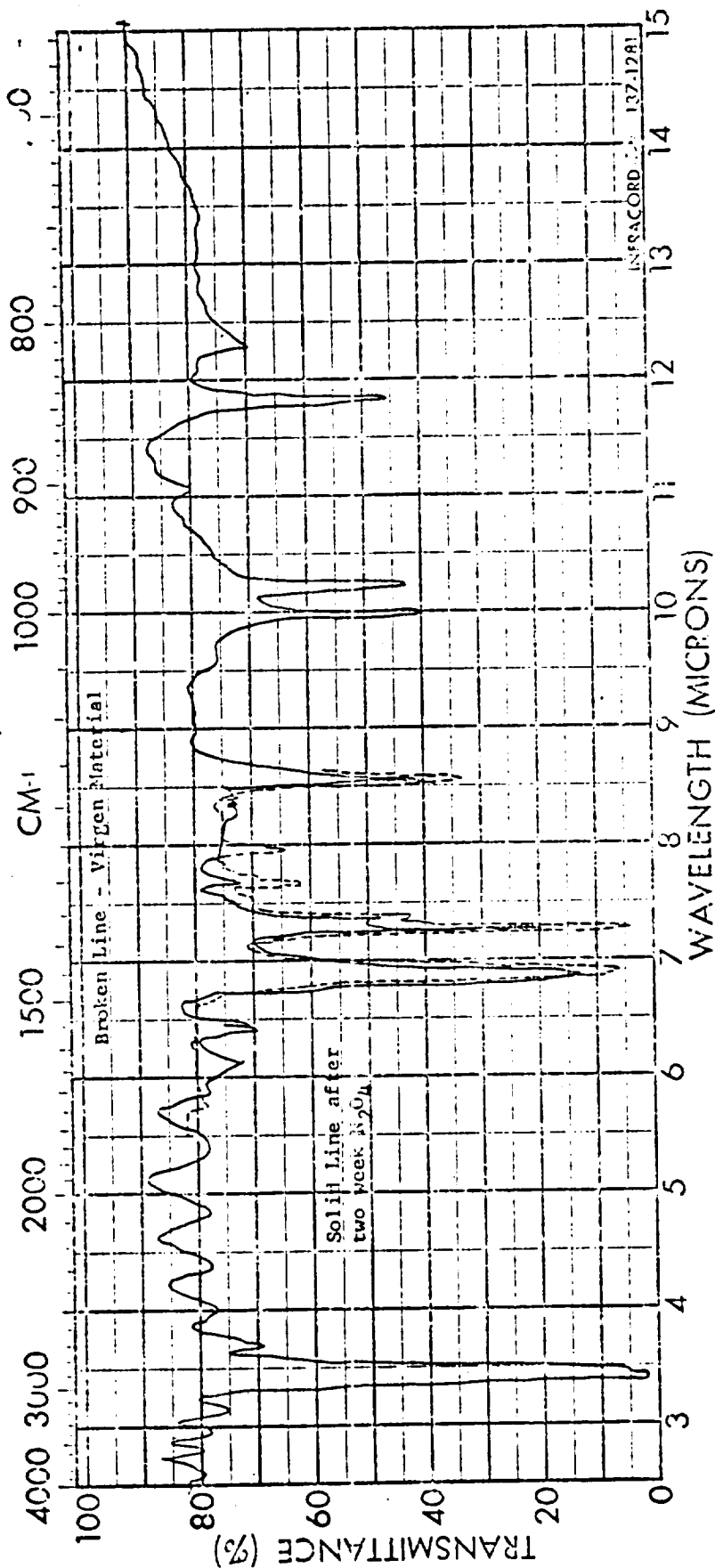




SPECTRUM NO. \_\_\_\_\_  
 SAMPLE \_\_\_\_\_

SPECTRUM NO. _____	ORIGIN _____	LEGEND _____	REMARKS line at 1700 _____
SAMPLE Kynar film	Pemisalt	1. Upper line - cured	and doubled at 1600 cm <sup>-1</sup>
comparison of incomplete cures	PURITY from dispersion 18	2. Lower line - incomplete cure	indicate IM phthalate
	PHASE film	DATE August 2, 1961	retention
	THICKNESS 2+ mils	OPERATOR Herb Fick	



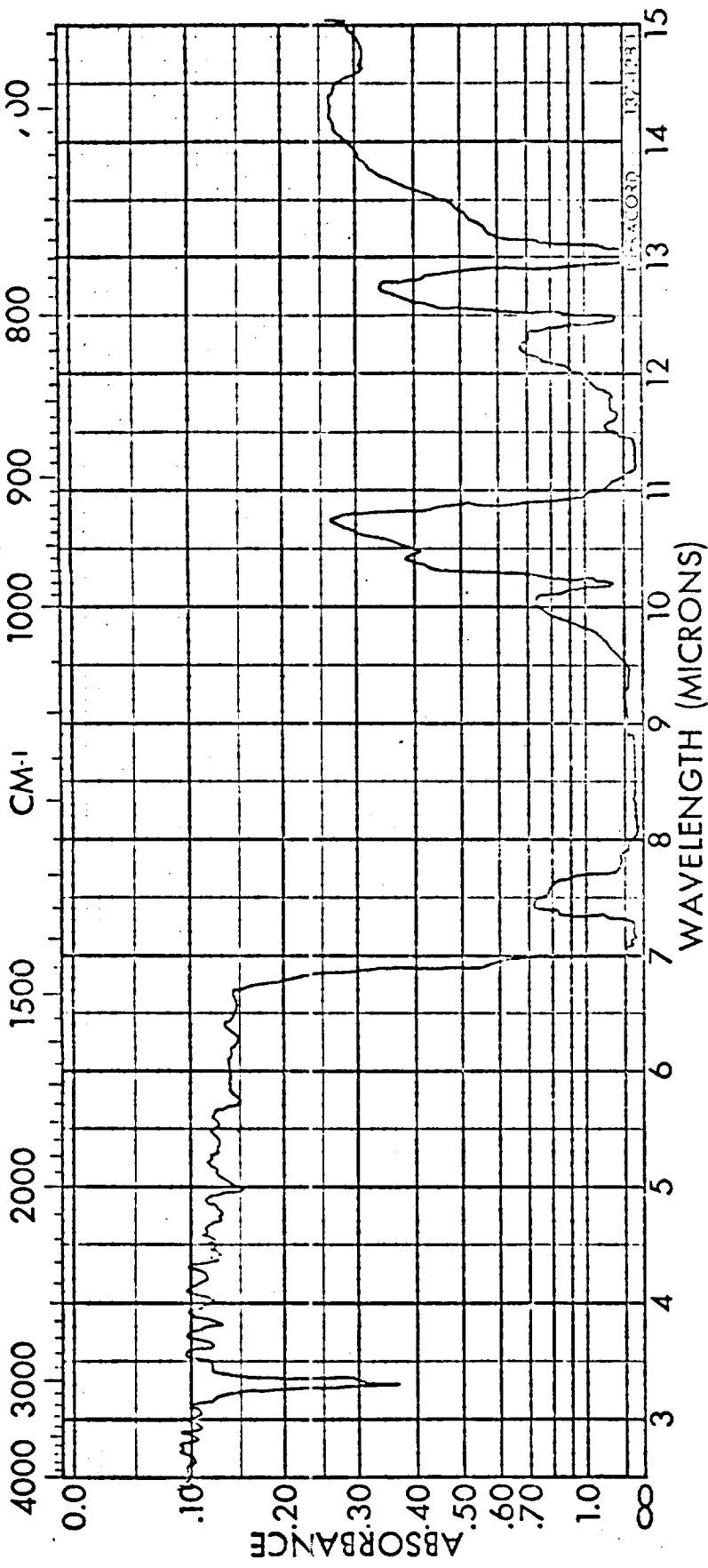


SPECTRUM NO. \_\_\_\_\_  
SAMPLE \_\_\_\_\_

SPECTRUM NO. x	ORIGIN Montecatini	LEGEND	REMARKS
SAMPLE Montecatini		1. Broken Line - Virgin Material	Possible absorption for NO <sub>2</sub>
Polypropylene after	PURITY Sample	2. Solid Line after 2 weeks N <sub>2</sub> O <sub>4</sub>	peak @ 1560. 1370 is masked
2 week immersion in N <sub>2</sub> O <sub>4</sub>	PHASE Film	DATE July 5, 1961	compare to Spectra 69
	THICKNESS 1 mil	OPERATOR Herb Fick	

THE PERKIN-ELMER CORPORATION, NORWALK, CONN.





SPECTRUM NO. \_\_\_\_\_  
 SAMPLE \_\_\_\_\_

SPECTRUM NO. _____	ORIGIN <u>Pennsalt Dispersion</u>	LEGEND _____	REMARKS _____
SAMPLE <u>Kynar</u>		1. _____	no 1700 or 1550 absorption
after 1 month in $N_2O_4$	PURITY <u>film</u>	2. _____	Sample allowed to lose
permeability app.	PHASE _____	DATE <u>August 2, 1961</u>	absorbed $N_2O_4$
	THICKNESS _____	OPERATOR <u>Herb Fick</u>	



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2. Letter to R. N. Porter - Jet Propulsion Laboratory, August 4, 1961
3. Letter to R. N. Porter - Jet Propulsion Laboratory, November 3, 1961
4. Proposal to Jet Propulsion Laboratory, February 6, 1961
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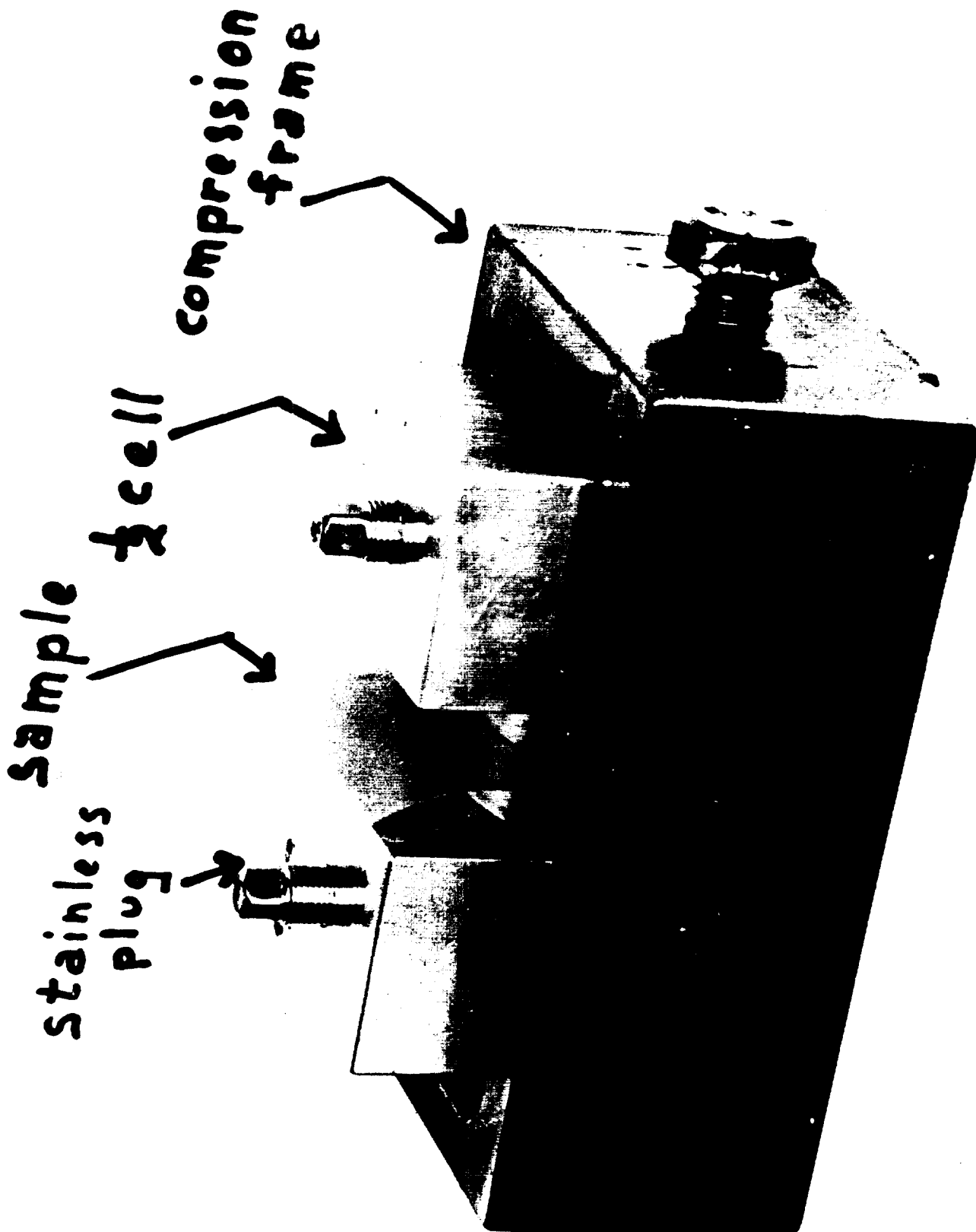
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17-A

NOT REPRODUCIBLE



TABLE II  
PHYSICAL PROPERTIES OF KYNAR GRADE 18

Property	Measurement	Unit	ASTM No.
Clarity	transparent to translucent		
Melting point, crystalline	340	°F	
Specific gravity	1.76		D792
Specific volume	15.7	in <sup>3</sup> /lb	
Refractive index, $n_D^{25}$	1.42		D542
Molding temperatures	400-550	°F	
Mold shrinkage, average	0.020	in/in	
Color possibilities	unlimited		
Machining qualities	excellent		
Flammability	self-extinguishing, non-dripping		
Tensile strength, 77°F	7000	psi	D638
Tensile strength, 212°F	5000	psi	D638
Elongation, 77°	300	percent	D638
Elongation, 212°F	400	percent	D638
Yield point, 77°F	5500	psi	D638
Yield point, 212°F	2500	psi	D638
Creep, 2000 psi, 77°F, 10,000 hrs.	0.02	in/in	
<i>See Figure 1</i>			
Compressive strength, 77°F	10,000	psi	D695
Modulus of elasticity, 77°F			
in tension	1.2x10 <sup>5</sup>	psi	D638
in flexure	2.0x10 <sup>5</sup>	psi	D790
in compression	1.2x10 <sup>5</sup>	psi	D695
Izod impact, notched, 77°F	3.8	ft-lb/in	D256
Izod impact, unnotched, 77°F	30	ft-lb/in	D256
Durometer hardness	80	Shore, D scale	
Heat distortion temperature, 66 psi	300	°F	D648
Heat distortion temperature, 264 psi	195	°F	D648
Abrasion resistance, Tabor			
CS-17, ½ kg load	17.6	mg/1000 cyc	
Coefficient of sliding friction to steel	0.14-0.17		
Thermochemical properties (estimated)			
1/n (CH <sub>2</sub> CF <sub>2</sub> ) <sub>n</sub> → CH <sub>2</sub> CF <sub>2</sub> (g) ΔH <sub>298</sub> <sup>o</sup>	+41.2	kcal	
1/n (CH <sub>2</sub> CF <sub>2</sub> ) <sub>n</sub> → 2C+2HF(g) ΔH <sub>298</sub> <sup>o</sup>	-12.0	kcal	
Thermal coefficient of linear expansion	8.5x10 <sup>-5</sup>	1/°F	D696
<i>See Figure 2</i>			
Thermal conductivity (Room temperature to 325°F) <sup>(2)</sup>	0.14-0.11	BTU/hr-ft-°F	
Specific heat	0.33	BTU/lb-°F	
Thermal degradation temperature	>600	°F	
Low temperature embrittlement	<-80	°F	
Water absorption	0.04	percent	D570
Moisture vapor permeability	1.0	g/mil-24 hr-m <sup>2</sup> -atm	
Radiation resistance (Co <sup>60</sup> )	>300x10 <sup>6</sup>	roentgens	

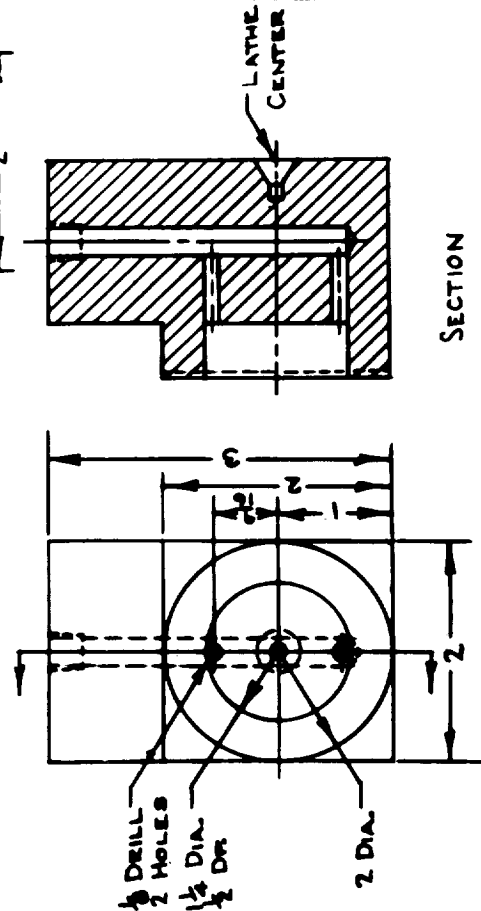
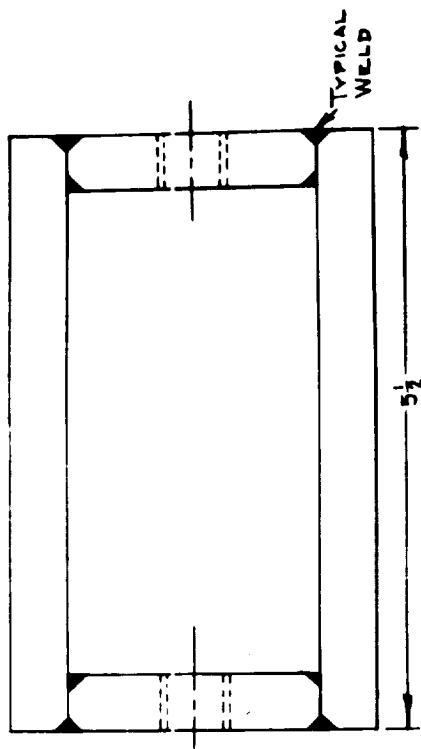


TABLE III  
CHEMICAL RESISTANCE OF KYNAR

Tensile strength of 5 mil. film immersed for 30 days at 122°F. in various chemical compounds. Unexposed control specimen tensile strength is 7200 psi.

	Chemical Compound	Tensile After Exposure (psi)		Chemical Compound	Tensile After Exposure (psi)
<i>Acids:</i>	Sulfuric, fuming	degraded	<i>Organic Compounds:</i> ( <i>Contd.</i> )	Carbon tetrachloride	6700
	Sulfuric, 95%	7100		Trichloroethylene	6700
	Nitric, fuming	6300		Ethylene dibromide	6500
	Acetic, glacial	5400		o-Dichlorobenzene	6200
	Hydrochloric 35%	7100		Chlorofluoroalkanes (e.g. Isotron® 113)	6900
	Sulfuric/hydrochloric 50/50	7300		Ethanol	6000
	Phosphoric 85%	7200		Ethylene glycol	7100
	Formic	6800		Phenol	5700
	Hydrofluoric 28%	6700		Ethyl acetate	5000
	Monochloroacetic	5400		Acetone	partially dissolved
<i>Bases:</i>	Sodium hydroxide 50%	7200		Acetophenone	5400
	Ammonium hydroxide	7200		Acetaldehyde	5200
	Diethylamine	5500		Benzaldehyde	5000
	Triethylamine	6400		Furfural	5000
	n-Butylamine	degraded		Dioxane	5200
	Aniline	5400		Nitrobenzene	5000
	Monoethylaniline	5600		Dimethylsulfoxide	partially dissolved
	Pyridine	4900		Dimethylacetamide	partially dissolved
	Hydrazine hydrate	7200			
	Hydrazine	5800			
	Unsymmetrical dimethylhydrazine	4700			
			<i>Other Chemicals:</i>	Chlorine (dry, 77°F)	7000
<i>Organic Compounds:</i>	n-Heptane	6500		Chlorine (wet)	7100
	Isooctane	6000		Bromine (dry, 77°F)	6700
	Kerosene	7100		Phosphorus oxychloride	4800
	Benzene	5600		Dinitrogen tetroxide	6500
	Toluene	5900		Hydrogen peroxide (90%, 77°F)	5500





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